

## Investigation of the Effect of Steel Plate Size and Elevated Temperature on Critical Load in Stability Tests

O.A. Pashkov<sup>1</sup>

<sup>1</sup>Moscow Aviation Institute (National Research University), Volokolamskoe shosse, 4, 125993, Moscow, Russia  
<sup>1</sup>oapashkov@mail.ru

**Article History** Received: 10 January 2021; Revised: 12 February 2021; Accepted: 27 March 2021; Published online: 28 April 2021

**Abstract :** This paper presents the results of a study of the effect of epoxy-polyester-based powder coatings on the critical strength of plate samples made of rolled sheet steel. The results obtained show that the model using flat elements gives a more accurate result than the model using three-dimensional elements. The best agreement with the experiment was shown by the results obtained in Ansys using the Eigenvalue bucling function, less than 1%. The worst agreement with the experiment was shown by the results obtained in Ansys using Solid elements, about 70%.

**Keywords:** Numerical modeling, coatings, strength, load.

### 1. Introduction

Preliminary experiments have shown that when studying the mechanical properties of samples of metal plates and metal plates with applied polymer coatings at elevated temperatures in stability tests, only the coated samples are affected [1-18]. Creation of polymer coatings on the surface of planar and spherical substrates becomes increasingly important and has attracted a great deal of attention of a gange of researchers [19-41]. Therefore, the purpose of this work was to perform a numerical and analytical calculation of the stability of samples of metal plates with polymer coatings. An analytical calculation was carried out for samples at room temperature using the Euler formula [42-44]. Numerical calculation was carried out in Ansys software for batches of samples at room and elevated temperatures [45-48].

### 2. Experimental studies of coating samples

Samples were considered from rolled sheet steel with a constant thickness of 0,7 mm and, depending on the batch, of various lengths and widths without coating and with it. Powder coating on epoxy-polyester base EUROPOLVERI (RAL 9010, Italy) with a thickness of about 250 microns with a spread of values of  $\pm 30$  microns was applied electrostatically. Before applying coatings, the steel surface was degreased and phosphated. Coating was carried out in a Gema paint booth (Switzerland). Drying was carried out at a temperature of 120 °C for no more than 5 minutes. Polymerization of the sprayed layer was carried out in a heat chamber at a temperature of 150 °C for 30 min. Samples were cooled in air for several hours.

The length of the working zone for specimens with a length of 240 mm was 131,85 mm, and for specimens with a length of 120 mm – 86,15 mm. For calculations, the length of the working zone was taken as 132 mm and 86 mm, respectively. The samples were tested at a constant speed of 0,5 mm/min. Mechanical grips were used for all samples. When tested with an elevated temperature, the sample was held for 10 minutes.

It was assumed that in the process of heating, the coated sample is weakened in the grips due to softening of the coating, and additional effort is required to fix the sample. For this confirmation, the effect of additional pulling up of mechanical grips was investigated in the stability test at elevated temperatures. The difference between the tests with and without pulling up consisted only in the fact that during the pull-up test the sample was additionally pulled up 5 minutes after reaching 80°C After additional tightening, the sample was kept for another 5 minutes at the same temperature. Samples without pulling up were kept at 80°C for 10 minutes. For this study, 6 samples were considered in each batch:

Uncoated batch with sample size 240\*24\*0,9

Coated batch and sample size 240\*24\*1

Uncoated batch with sample size 120\*24\*0,9

Coated batch and sample size 120\*24\*1

This study showed the need for additional pull-up of coated samples. Therefore, all other coated samples were tightened after 5 minutes at a temperature 80 °C.

Twelve batches were considered to study the effect of the coating on the critical force in the elevated temperature test. Each batch consisted of 5 samples, each sample was kept at a temperature of 80°C for 10 minutes. The coated lots were additionally pulled up. The following batches have been tested:

Uncoated batch with sample size 240\*24\*0,7  
 Coated batch and sample size 240\*24\*1,2  
 Uncoated batch with sample size 120\*24\*0,7  
 Coated batch and sample size 120\*24\*1,2  
 Uncoated batch with sample size 120\*12\*0,7  
 Coated batch and sample size 120\*12\*1,2

Mechanical tests were carried out on an Instron 5969 setup (UK) with Bluehill 3 software. For numerical simulation of buckling tests, standard methods of finite element analysis in the Ansys system were used.

### 3. Methods and results of numerical modeling

In the calculations, the following values of the physical and mechanical properties of the samples were used:

Sheet steel: Elastic modulus  $E = 200$  GPa, Poisson's ratio  $\mu = 0,3$ , Coefficient of thermal expansion  $\alpha = 12,5 * 10^{-6} \text{C}^{-1}$ , EUROPOLVERI coating: Elastic modulus  $E = 3$  GPa, Poisson's ratio  $\mu = 0,03$ , Coefficient of thermal expansion  $\alpha = 55 * 10^{-6} \text{C}^{-1}$ .

In the numerical calculations, the possible curvature of the sample was taken into account by setting the initial curvature by the radius. When calculating for an elevated temperature, polymerization at a temperature of  $150^{\circ}\text{C}$  was taken into account, taking the temperature change relative to the neutral state equal to  $-70^{\circ}\text{C}$ .

Ansys built a curved surface with a curvature of a radius of  $1 * 107\text{mm}$ . Two variants of modeling experimental samples were considered: by two-dimensional modeling: the surface was broken by two-dimensional QUAD elements; and 3D modeling: solid was broken by 3D Hex elements. To simulate anchoring similar to the experiment, the boundary conditions were set: The lower face was set to the termination conditions (prohibition of displacements and turns in all directions). The conditions for prohibiting displacements in the direction of the width  $O_x$  and thickness  $O_z$  of the sample, as well as rotation around the direction of the width of the sample  $R_x$ , were set on the upper face. The load was applied to the upper face along the  $O_y$  axis in the form of a force. The coverage was modeled by the layered section function.

The value of the critical force is determined from the formula of the theory of bar stability for the case of vertical load action and rigid pinching of the ends of the bar:

$$P_{kp} = \frac{4\pi^2 EJ}{l^2},$$

where  $l = 86$  mm – rod length,  $E$  – Young's modulus,  $J$  – moment of inertia of the cross-section of the bar.

When modeling plates without coatings, we take  $E = E_{cm}$  – Young's modulus of steel,  $J = J_{cm} = bh^3/12$  – moment of inertia of samples with thickness  $h$  and width  $b$ . When modeling plates with coatings, the stiffness of the corresponding bar in bending should be calculated taking into account the additional contribution from the coating layers:  $EJ = 2E_n J_n + E_{cm} J_{cm}$ , where  $E_n$  – is the modulus of elasticity of the coating,  $J_n$  – is the moment of inertia of the coating layers displaced relative to the neutral line of the bar. However, the use of such a refined estimate leads to an insignificant change in the calculated critical load (within 2%), which cannot explain the obtained experimental data. Therefore, the graphs show the only value of the critical load, calculated without taking into account the effect of coatings.

The dependence of the curvature of the sample on the critical load is shown in the figure 1.

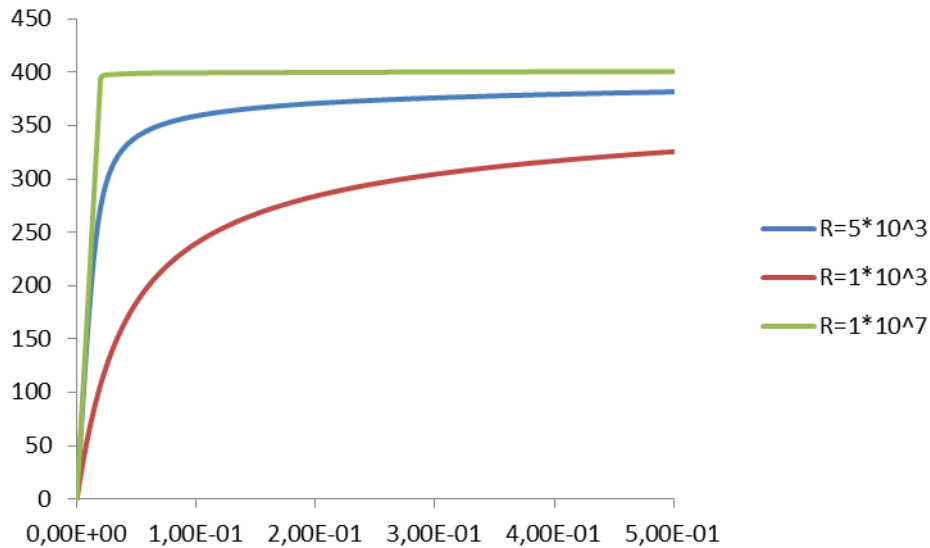


Fig. 1. Dependence of the critical load on the given curvature of the specimen for a specimen measuring 120\*12 mm.

The effect of coating thickness on the critical force of the sample is shown in the figure 3.

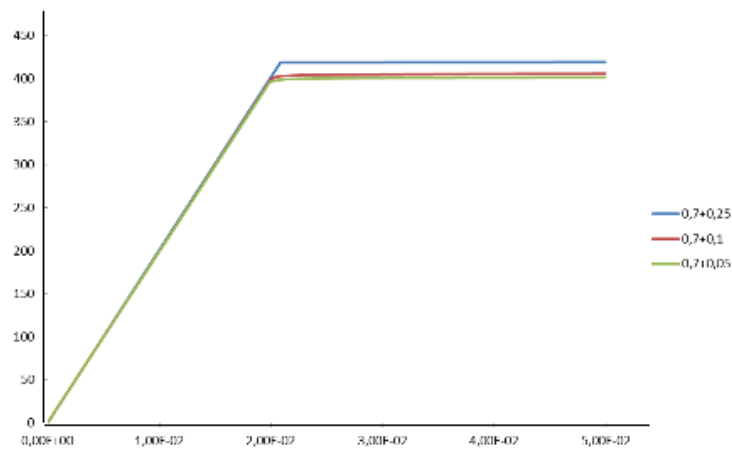


Fig. 2. Influence of coating thickness for samples 120\*12.

The difference between the results obtained numerically and the experiments was substantiated, namely, the slope of the load-displacement curve. The figure below shows the experimental results and numerical results using flat and three-dimensional elements.

To check the numerical calculations, an analytical dependence was obtained:

$$U = \frac{P}{S_{\Sigma}E} L,$$

where U- displacement, P-load, L length of the working part, E - elastic modulus,  $S_{\Sigma}$  sample area. Shown in green on the graph.

The results for coated samples are given in Figure 3 and 4.

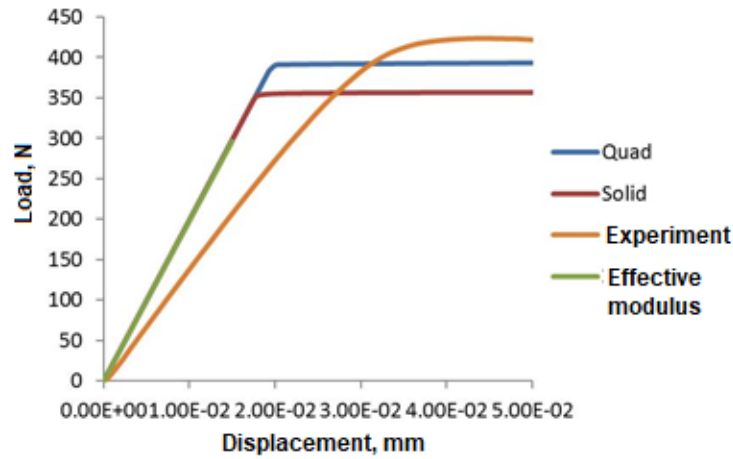


Fig. 3. Experiment results.

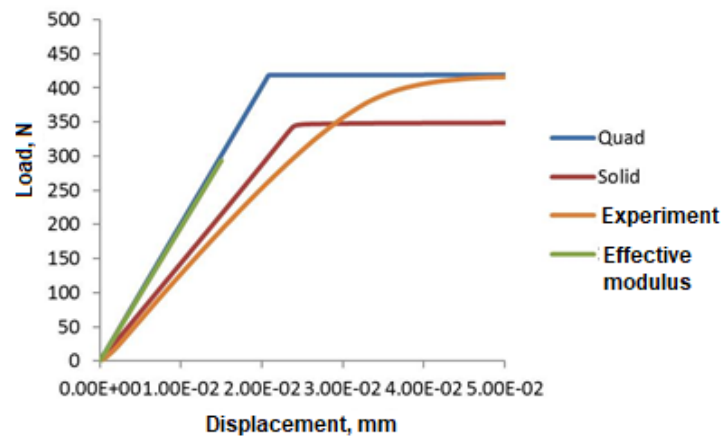


Fig. 4. Results of a numerical experiment.

As can be seen from Fig. 4, the value of the inclination angle obtained analytically coincides with the results obtained numerically using flat elements. The results obtained using three-dimensional elements differ significantly. It could be due to accumulating error.

This result shows that a model using flat elements gives a more accurate result than a model using three-dimensional elements.

The best agreement with experiment was shown by the results obtained in Ansys using Eigenvalue bucling, less than 1%. The worst agreement with the experiment was shown by the results obtained in Ansys using Solid-elements, about 70%.

**4. Conclusion**

The numerical results obtained for different elastic moduli showed that the deviation of the numerical curve from the experimental one is associated not with the physical and mechanical properties and geometric characteristics of the sample, but with the results obtained. Because the change in the displacement of the end of the sample was measured along the traverse, then the slope of the curve in this situation may not be true, and may not coincide with the slope obtained numerically. Also here one should take into account the fact that the loading rate of the sample was 2 times less than the loading rate to determine the elastic modulus.

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