A Study on the Manufacturing of Molybdenum Pins for Electrodes

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Abstract: The molybdenum cup and molybdenum pin, which are the main materials of the molybdenum electrode used for the LCD BLU CCFL electrode, have not been developed in Korea and imported from Japan. In this paper, especially, research on prototype manufacturing and CAE analysis is performed to develop a molybdenum pin. In this research, to develop the manufacturing technology of molybdenum pin used for CCFL electrode of LCD BLU, development of linear processing technology, development of molybdenum wire surface treatment technology, development of wire cutting technology, production of molybdenum pin, design and fabrication of JIG and Fixture for inspection, molybdenum pin prototyping and analysis, and development of 100% molybdenum pin inspection technology. The development of molybdenum pins developed through this research can overcome Japan's technological level, which depends entirely on imports from Japan, and it is thought that the development will have a significant impact on the overall industry using molybdenum pins.

Keywords: Molybdenum pin, LCD, BLU, Prototype manufacturing, CAE analysis.

Introduction
Backlights are used as materials for a variety of home appliances and light sources, and are broadly divided into LED, CCFL and EEFL. Among them, CCFL can be said to be the most versatile backlight. Compared to the EEFL, CCFL has a simpler production process and outperforms LED in terms of price. It is also widely used not only in home appliances but also in fields such as electronic bulletin boards. [1, 2] Liquid Crystal Display (LCD), a type of thin display, has advantages in terms of power consumption and mobility, and will continue to drive growth centered on general-purpose displays. Figure 1 is the BLU structure used for TV. [3-5] CCFL, which serves as a light source for LCDs, is similar to general fluorescent lamps, but has the advantage of being small in size, high in brightness, and long service life. [6, 7] CCFL and electrode rod structures are manufactured by welding Durmet to Kovar pins as shown in figure 2 and laser welding or resistance welding to Ni cups where glass is beaded. A nickel electrode composed of Kovar pins and Ni cups is changed to molybdenum electrodes (combination of molybdenum cups and molybdenum pins) according to CCFL brightness and life requirements. [8-10] The molybdenum cup and pins, which are the materials for molybdenum electrodes, are not processed in Japan and are imported from Japan in all quantities.
In this task, we studied the manufacturing process of molybdenum pins for LCD and conducted research on the development of linear processing technology, molybdenum wire surface treatment technology, wire cutting technology, design and manufacture of JIG and Fixture for manufacturing and inspection of molybdenum pins, prototype and analysis of molybdenum pins, and development of full number inspection technology of molybdenum pins. [11, 12]

1. CCFL Technology Development and Details

A molybdenum pin is made of a molybdenum wire having a diameter of 1.0 mm or more. Molybdenum pinning processing goes through the following steps. It consists of straightening technology, cutting technology, surface treatment technology, and finally total inspection technology. In this study, the ultimate goal is to develop an automated process that enables the production and inspection of molybdenum pins.

During the manufacturing process, minor changes in the external environment can cause defects such as cracks in materials, which can cause serious failures in the performance of CCFL products and therefore require quality assurance and full-scale inspection. Figure 3 is a magnified view of fine cracks on molybdenum pins, and figure 4 shows the occurrence of defective leaks on fine cracks.

![Figure 3. Small crack magnification of molybdenum pin](image)

![Figure 4. Bad leak occurrence of small crack (Penetrant experiment)](image)

For the ultimate development goals of this research, technology development is necessary according to the following procedures. The first linear treatment technology determines equipment design for a linear machine of a high-speed rotating method, linear machine optimum machining conditions for optimum linear molding, linear treatment technology development for molybdenum wire including centerless grinding processing, the second molybdenum wire surface treatment technology development includes removal of foreign substances such as graphite used when drawing molybdenum wire, conditions and technology development for surface friction processing for surface treatment, the third involves development of bundling technology for minimizing material deformation, and linear design of molybdenum wire for manufacturing and inspection. Fifth is the prototype and analysis of molybdenum fins, the thermal transfer analysis of molybdenum fins, and the three-dimensional precision measurement of molybdenum fins. Finally, the development of the whole inspection technology of molybdenum fins means the development of the whole inspection technology of molybdenum fins and the development of equipment.

2. Experimental Manufacturing at molybdenum pin, 3D precision measurement and CAE analysis

2.1. Molybdenum pin manufacturing

Among the various molybdenum pin standards, a production schedule standard was made and shown in figure 5 below.
2.2. Molybdenum pin prototype speculation

The standards for molybdenum pin prototypes shall be within the dimensional tolerance range of parts A, B, and C, and the surface gloss and surface illuminance shall be equal to or greater than those of products currently in use. In contrast, the standards for A, B, and C and the prototype standards for tolerance are shown in figure 6.

![Figure 6. Specification of prototype](image)

<table>
<thead>
<tr>
<th>Class</th>
<th>A</th>
<th>B</th>
<th>C</th>
<th>Remark</th>
</tr>
</thead>
<tbody>
<tr>
<td>Spec.</td>
<td>0.8mm</td>
<td>3.3mm</td>
<td>0.2~0.3</td>
<td></td>
</tr>
<tr>
<td>Allowance</td>
<td>±0.02</td>
<td>±0.1</td>
<td>-</td>
<td>-</td>
</tr>
</tbody>
</table>

2.3. Molybdenum pin prototype inspection report

The results of the first prototype were found to be improved, and after additional improvement work, the second prototype was produced. The report of the prototype is shown in figure 7.

![Figure 7. Prototype certification of the first time and the second time](image)

2.4. Molybdenum pin 3D precision measurement

There are three methods of molybdenum pin 3D precision measurement: 3D-CT imaging of the first prototype, laser confocal microscopy, and X-Ray imaging. First, 3D-CT photography is to confirm the epicenter of molybdenum pins after centerless processing, and the epicenter measurement of the prototype is shown in figure 8.
For precision impression of laser confocal microscope (metal microscope), the depth value of Crack was measured by scanning the shape of Z axis in the depth direction with Laser and realizing the image taken by tomography in 3D. (Minimum unit: 0.001 μm) The test crack depth measurement of a metal microscope is shown in figure 9.

Finally, for the X-ray photography, X-ray photography was performed for the purpose of microcrack inspection inside molybdenum wire, and the presence or absence of Crack was determined and shown in figure 10.

Comparing these dimensions, the total length, outer diameter, and corner rounding (R) dimensions are different. For comparison of electrical dimensions, the standard tolerance was evaluated on the basis of 3.30±0.1 mm. Both Cp and CpK are insufficient due to the large variation and the average deviation of the primary prototype to the lower limit (3.20 mm) of the standard, and some of the products are out of the lower limit of the standard. The secondary prototype was manufactured to be distributed to the standard size (3.30 mm) by improving the cutter, and both Cp and CpK are good, and the comparison of the prototype’s total length histogram and distribution diagram is figure. It seems to be figure 11.
In the outer diameter dimension comparison, the standard tolerance is evaluated on the basis of $\phi 0.80 \pm 0.02$ mm. Although the first prototype is located on average at a slightly lower limit, the variation in the total length of the prototype is small, and both $C_p$ and $C_Pk$ are of a normal level. The secondary prototype is located at a slightly upper limit and close to the standard $\phi 0.80$. Comparison of the outer diameter histogram and distribution map of the prototype is figure 12.

Corner rounding (R) dimension comparison is as follows: The standard tolerance shall be evaluated on the basis of 0.2-0.3 mm. The size of the first prototype was about 0.13 millimeters, and it became the shape of the epicenter. The second prototype was made in an elliptical corner round shape similar to the current product for sale, and the size was maintained to be more than 0.2 mm. The projector comparison measurement for corner rounding(R) dimension comparison is figure 13.

There is a comparison of appearance by optical microscope and SEM. A comparison of appearance by optical microscope shows that the primary prototype does not have a flat cut surface and includes oblique products. As a result, it was not possible to completely remove the scratch on the cross section that occurred during cutting. The second prototype was made flat by improving the conditions of precision cutters. Figure 14 is a comparison of optical microscopes of the first and the second prototypes.
In the comparison of appearance by SEM comparison, residual foreign substances are attached to the primary prototype after the surface treatment. Although no extreme difference is seen in the comparison of the secondary reflection electron commercial surface unevenness, it can be confirmed that surface scratch remains on the cut surface in the comparison of the cross section. In the secondary prototype, the remaining foreign substances were removed by ultrasonic cleaning, and the surface scratch of the cut surface was removed by changing the conditions of the precision cutter. The comparative photography of the first and second prototype by SEM is Fig. It is shown in figure 15.

![Figure 15. Comparison shooting of SEM](image)

The second prototype was applied to complement the problems arising from the first prototype, and the improvements made by this study were as follows: Firstly, in the case of the number of electrical devices, the hexagon is maintained constant by changing from the Hand Swaging multiple flux system to the Press Swaging system, and no change in wire straightness occurs, and no distortion occurs in precision cutting, thereby reducing the deviation of the length. A micrometer header is additionally mounted on the precision cutter so that the micrometer header can be finely adjusted up to 0.01 mm. In the case of the outer diameter dimension, the RPM value and working time of the high speed barrel polishing machine are corrected. The RPM of the first prototype was increased by about 10%, and the working time was reduced by about 5%. (125 RPM, 17 hours) Third, in the case of appearance, vinyl containers were stored after drying after high-speed barrels and after natural drying. However, when the second prototype was manufactured, the containers were washed with ultrasonic waves and dried with an electric dryer in order to remove foreign substances. The containers were sealed and stored in storage. In addition, the scratch of the surface cross section is improved by changing the conditions of the high-speed burrel polishing machine and the precision cutting machine, respectively.

2.6. Molybdenum pin heat transfer analysis

In analyzing CCFL with ANSYS, if conditions are given according to the material properties first, it is found through analysis that the temperature of the cup made of nickel or molybdenum is the highest if the temperature of the cup part is shown to be close to 500°C at room temperature, the temperature is slightly lowered by pins, and the temperature of the Dumet part made of the synthesis of nickel and manganese is lowered as it moves away from the cup. The CCFL heat transfer analysis for these is as follows.
3. Conclusions

Because molybdenum pins are manufactured on CCFL electrodes of LCD backlight, precise processing and inspection are difficult due to material problems, so research on uniform production is needed. In this study, a molybdenum pin was prototype, and after 3D precision measurement of the molybdenum pin, heat transfer analysis was performed at the end to prove its validity. First of all, after the first trial, additional improvement work was carried out to develop a prototype satisfying the standards. Secondly, molybdenum pin 3D precision measurement methods were used to measure the depth of cracks in the prototype and to experiment with microcracks using a metal microscope among 3D-CT photography, laser control microscopy, and X-Ray photography. Through the production of the first and second prototypes, a comparison of full length dimensions, a comparison of outer diameter dimensions, and a comparison of corner-rounding dimensions were also conducted, and the distribution chart of the full length was shown in histograms. Corner Rounding compared SEM with an optical microscope and proved that the secondary prototype was highly complete. Thirdly, CCFL conducted CAE analysis through ANSYS and confirmed that when cup parts made of nickel or molybdenum show temperatures close to 500°C to DP at room temperature, the temperature drops slightly at the pin, and in Dumet parts made of nickel and manganese synthesis, the temperature drops further away from the cup. The research is part of the production stage of molybdenum pins.

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References