

## Integrating VLSI Design Strategies to Optimize Signal Equalization and Power Supply Modulation (DELTA-SIGMA)

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**Abstract:** This research investigates the application of Delta-Sigma Modulator controlled switch-mode power supplies to address the challenges associated with conventional PWM-controlled DC-DC Buck Converters. By exploiting the noise-shaping capabilities of Delta-Sigma modulation, in-band tones in the output are mitigated. The study encompasses three phases: initial design and performance evaluation of PWM-controlled converters, transition to Delta-Sigma Modulator control, and refinement of the design to enhance efficiency and noise performance. Notable achievements include reducing inductor values and integrating on-chip capacitors, leading to a peak efficiency of 91% at a 200MHz sampling frequency. Post-layout simulations further validate the superiority of Delta-Sigma Modulator controlled switch-mode power supplies over PWM-controlled counterparts.

**Keywords**—Output Voltage, Duty Ratio, Load Resistance, Efficiency, Control Voltage of the switches, Ripple Voltage, Input Voltage, FFT, layout, Inductor loss, Additive quantization noise, DDR2-SDRAM, time-to-digital conversion, PVT, FSM and Control Circuit.

### I. INTRODUCTION

The relentless pursuit of efficiency and reliability in electrical systems has prompted researchers to explore innovative approaches to power supply design. Central to this endeavor is the development of DC-DC converters capable of converting electrical power with minimal noise and maximum efficiency. Conventional PWM-controlled converters, while prevalent, exhibit limitations such as output voltage ripple and in-band tones, which undermine performance and reliability. This research sets out to address these challenges by investigating Delta-Sigma Modulator controlled switch-mode power supplies as a promising alternative. By leveraging the noise-shaping properties of Delta-Sigma modulation, this study aims to mitigate noise and enhance overall performance. Through a systematic three-phase methodology involving design, modification, and evaluation, this research seeks to advance the state-of-the-art in power supply technologies. The anticipated outcomes include improved efficiency, reduced noise levels, and enhanced reliability, thereby catering to the evolving demands of modern electrical systems.

Through mathematical modeling and simulation, we present the performance enhancement of Delta-Sigma Modulator controlled switch-mode power supplies over PWM-controlled counterparts. Our design achieves a remarkable 91% peak efficiency, with noise levels reduced by approximately 35dB at the 43rd harmonic. By optimizing inductor values and sampling frequency, our approach demonstrates superior noise performance and efficiency, validating its efficacy in modern power supply systems.

### II. EXPERIMENTAL PRINCIPLES

#### A. Controller for the control of dc-dc buck converter

1) *PWM controller:* It can be expressed as

$$S_{V_{ctrl}^{ss}} = \frac{F\{V_{ctrl}^{ss}\}^2}{Re\{Z_{out}\}} = (2\pi D)^2 \text{sinc}^2\left(\frac{\omega DT}{2}\right) \sum_{n=-\infty}^{\infty} \delta\left(\omega - \frac{2*\pi*n}{T}\right) \tag{7}$$

where  $S_{V_{ctrl}^{ss}}$  is the PSD of  $V_{ctrl}^{ss}$ .

2)  $\Delta\Sigma$  modulator-based controller: The output is defined by the following equation

$$Y = Xz^{-2} + N(1 - z^{-2}) \tag{8}$$

where X is the input signal and N is the additive quantization noise.

#### B. Control schemes of dc-dc buck switching converters

- To ensure stable loop response of the switching converters, the usual practice is to design for a gain of at least 6 dB and phase margin of at least 45°. Under this condition second order system would have critically damped step response.

- For the system to be stable the unity gain crossover frequency must be half of the switching frequency. This ensures Nyquist Sampling Theory.
- Even the unity gain crossover frequency should be high enough to allow the switching converter to respond quickly to its output transients.
- Having set the unity gain crossover frequency, the gain of the error amplifier is selected to yield a total loop gain of 0 dB at unity gain crossover frequency.
- The magnitude response of the error amplifier is designed to cross 0 dB at a slope of (-) 20 dB/decade with desired gain margin.

Transfer Function of this passive filter

$$\frac{V_o(s)}{V_{in}(s)} = \frac{R}{L * C * R * s^2 + s * L + R} \tag{9}$$

Where  $R_{csr}=0$ . For PID compensator has 3 poles and 2 zeros. The integration provided by the 3<sup>rd</sup> pole, located at zero, which is used to minimize the steady state error.

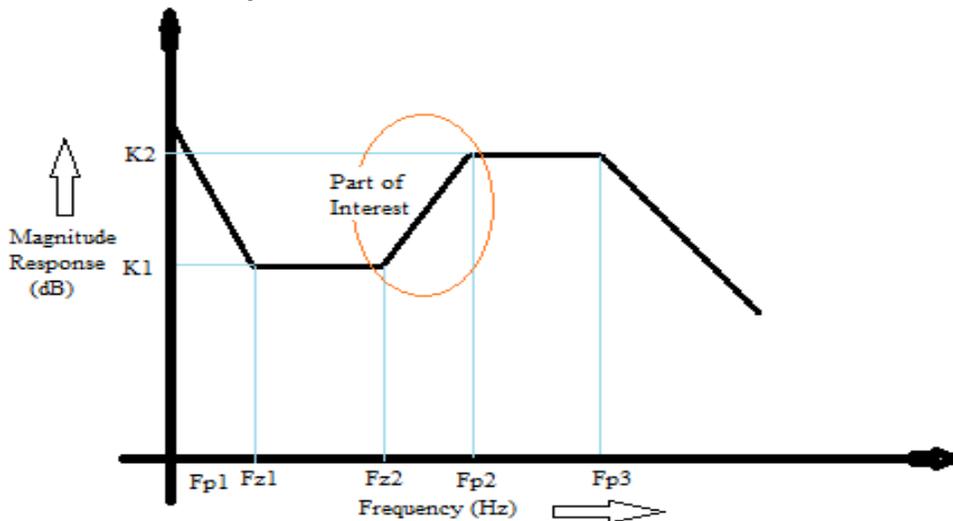


Fig. 3. PID Compensator magnitude plot

➤ Importance of Error amplifier compensator:

It is required because switching converter can be stabilized by adding a compensator network in the error amplifier to increase the phase margin. Transfer function of the output filter:

$$\frac{7.26}{4.4e^{-14}s^2 + 2e^{-6} + 11} \tag{10}$$

### III. DESIGN & OPERATION OF SYSTEM

#### A. DELTA SIGMA MODULATOR controlled DC-DC Buck Converter

Delta-Sigma Modulator controlled DC-DC Buck Converter produces a fixed period varying-frequency pulse waveform known as pulse code modulation (PCM).

- Input Voltage: 5V
- Output Voltage: 3.3V
- Required duty cycle is  $D = 3.3/5 = 0.66 = 66\%$
- Operating frequency: 200 MHz
- Load resistor is kept at the value of  $R_{out} = 11 \Omega$
- Output current = 300 mA.

1) Selection of Inductance (L):

Sampling frequency =  $F_s = 200M$  Hz.

$$\Delta I = \frac{V_{out}(1-D)T_s}{L} \tag{17}$$

$\Delta I$  = peak to peak current ripple in the inductor.

We are operating the converter in continuous mode of operation. Chosen,  $\Delta I=2.8\text{mA}$

- The value of  $L=2\mu\text{H}$

2) Selection of corner frequency of the output filter( $F_c$ ),load capacitance ( $C_{out}$ ):

$$\frac{\Delta V_{out}}{V_{out}} = \frac{\pi^2(1-D)}{2} \left(\frac{F_c}{F_s}\right)^2 \tag{18}$$

Chosen,  $\Delta V_{out} = .877\text{ mV}$

- The value of  $F_c=2.51646\text{MHz}$

$$F_c = \frac{1}{2\pi\sqrt{L C_{out}}} \tag{19}$$

The value of  $C_{out} = 2\text{ n F}$

3) Design of Attenuator:

The sampling network,  $R_1$  and  $R_2$ , contributes an attenuation according to its sampling ratio  $R_2/(R_1+R_2)$ . The gain attenuation of the sampling network is  $20\log(0.9/3.3) = (-) 11.285\text{dB}$ . The chosen value of  $R_1=24\text{K}$ ,  $R_2=9\text{K}$

4) Design of  $\Delta\Sigma$  modulator block:

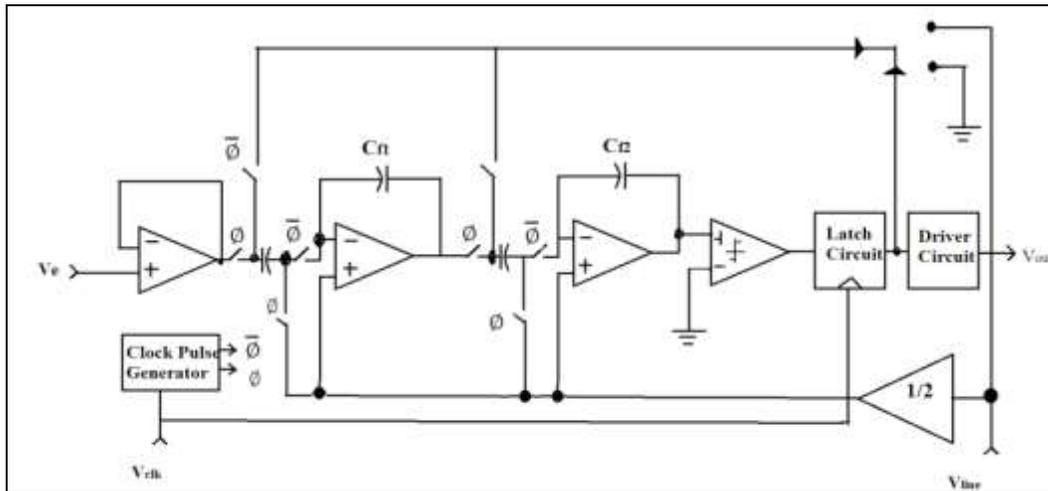


Fig. 6. Switched-capacitor  $\Delta\Sigma$  modulator

$C_{S1}\&C_{S2} = 0.5\text{pF}$ ;  $C_{f1}\&C_{f2} = 1\text{pF}$ .

- The low frequency gain of the open loop buck converter is  $(8.87-11.285) = (-)2.415\text{dB}$

5) Design of compensator:

Unity gain crossover frequency ( $F_1$ ) = (1/5th of switching frequency ( $F_s$ )) = 20MHz

Transfer function of the output filter:

$$\frac{7.26}{4.4e^{-14}s^2 + 2e^{-6} + 11} \tag{20}$$

Hence the gain of the error amplifier should be chosen to be  $(-)(-22.745-2.415) = 25.16\text{dB}$ .

- $R_B/R_A = 1.81$
- Let,  $R_A = 1\text{K}\Omega$
- $R_B = 1.81\text{K}\Omega$

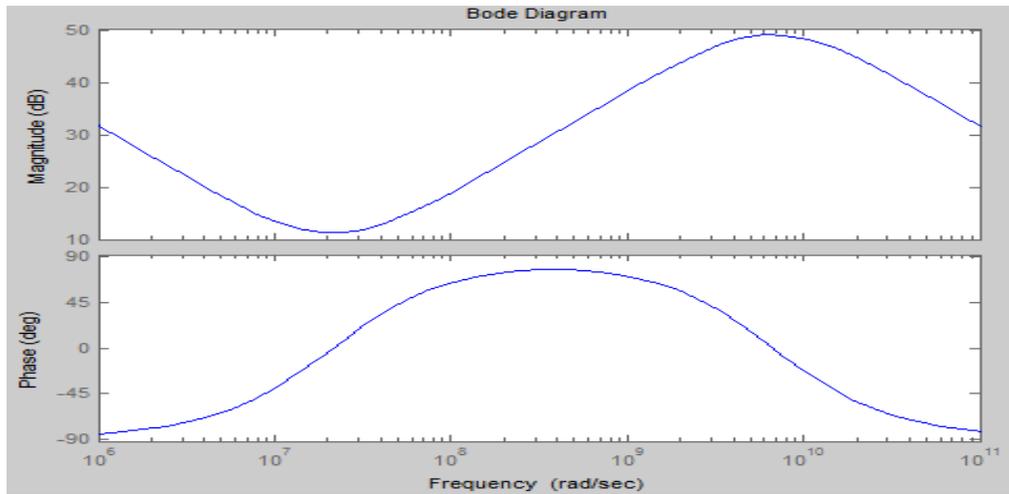


Fig. 7. Gain and Phase plot of PID compensator

Transfer function & bode plot of the compensator

$$\frac{2.187e^{-15}s^2+9.352e^{-8}s+1}{5.666e^{-28}s^3+7.663e^{-18}s^2+2.591e^{-8}s} \tag{21}$$

*B. Design of OP-AMP*

It is basically design on rail to rail operation.

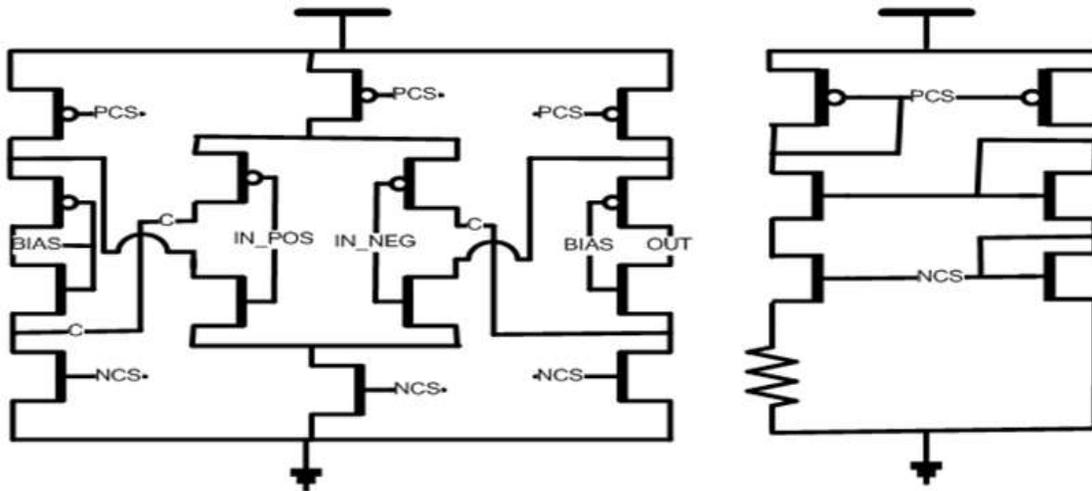


Fig. 8. Op-amp Circuit

C. Design of dynamic comparator

The latched comparators work synchronously with the sclock signal and indicate, through their digital output level, whether its differential input signal is positive or negative. They use a positive feedback mechanism to regenerate the analog input signal into a full scale digital signal (regenerative amplification).

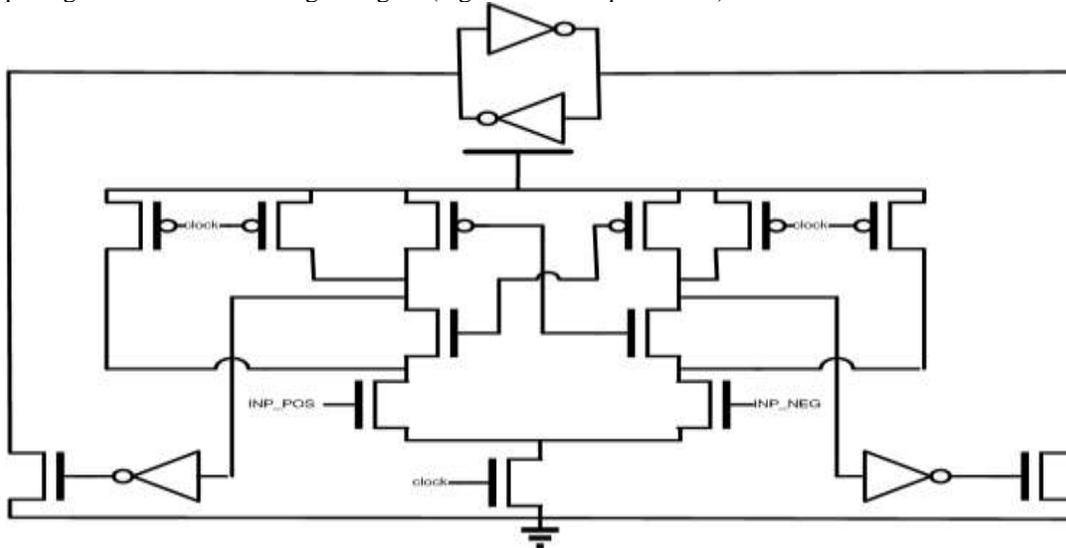
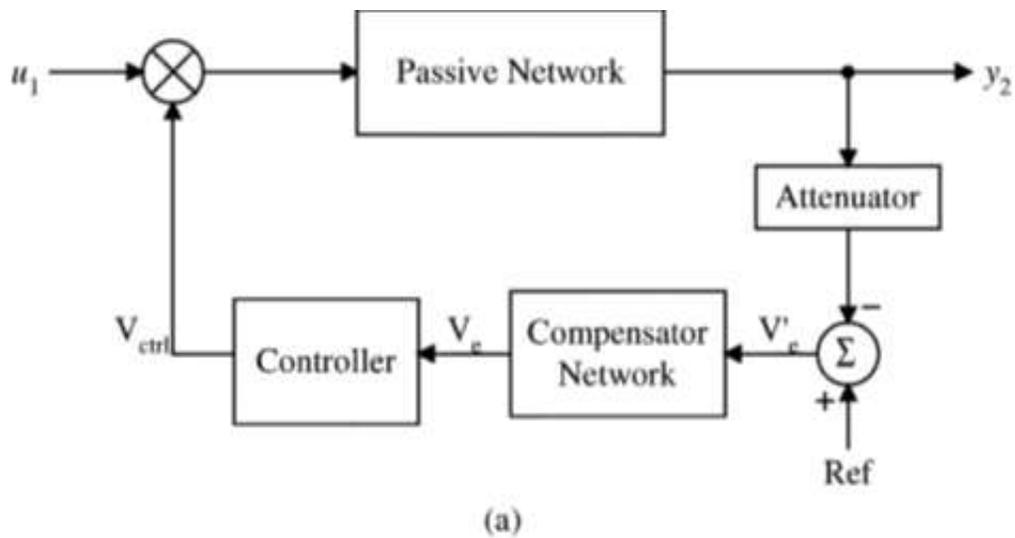


Fig. 9. Dynamic comparator

IV. EXPERIMENTAL RESULTS



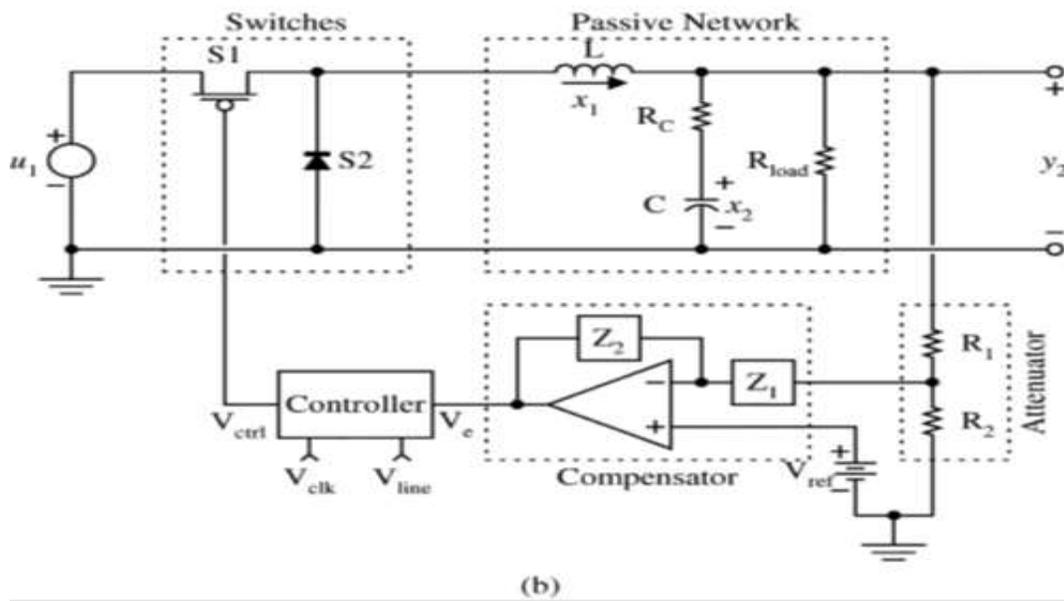


Fig. 15. Typical buck-type SMPS. (a) Block diagram (b) Circuit diagram

1) PWM controller-based Dc-Dc Buck Converter:

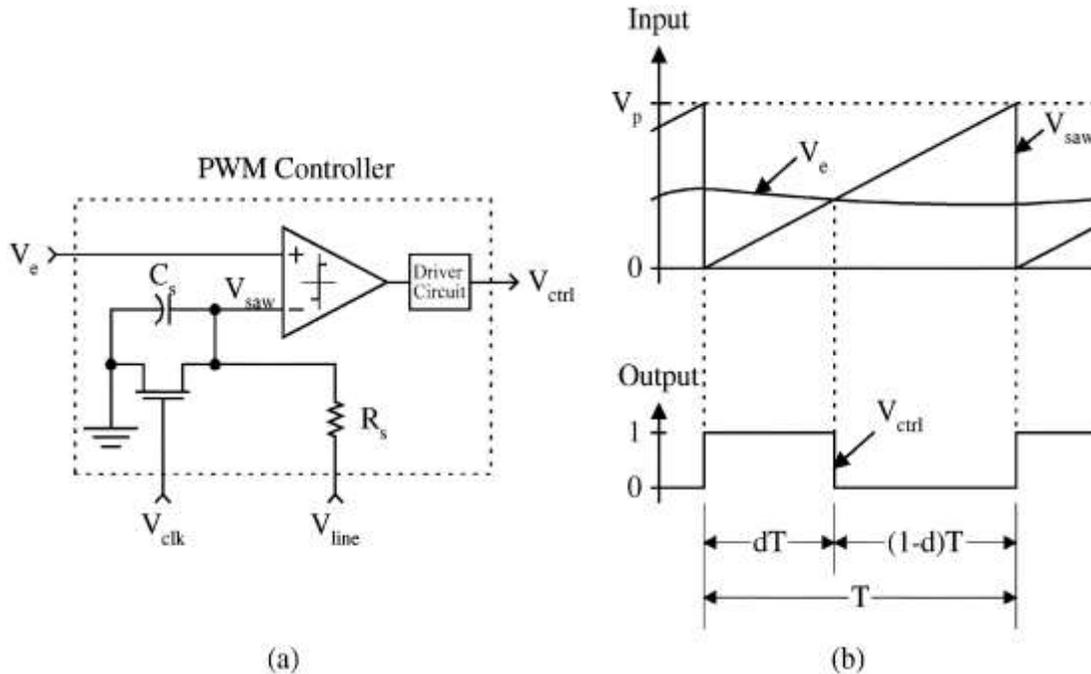


Fig. 16. PWM Controller (a) Circuit diagram (b) Input and output waveforms

- Overshoot: (3.671-3.075) V
- Settling Time: 46.92us
- Ripple at Vout: (3.302-3.295) V
- Efficiency: 79%
- FFT Spectre:

Signal (5MHz): (-) 46.76 dB  
 2<sup>nd</sup>Harmonic: (-) 72.05 dB  
 4<sup>th</sup>Harmonic: (-) 74.24 dB  
 6<sup>th</sup>Harmonic: (-) 85.98 dB  
 (-) 85.48 dB

1<sup>st</sup>Harmonic:(-)57.19dB  
 3<sup>rd</sup>Harmonic:(-)75.23dB  
 5<sup>th</sup>Harmonic:(-)82.68dB  
 7<sup>th</sup>Harmonic:(-)81.29dB  
 9<sup>th</sup>Harmonic: (-) 107.7 dB

8<sup>th</sup>Harmonic:

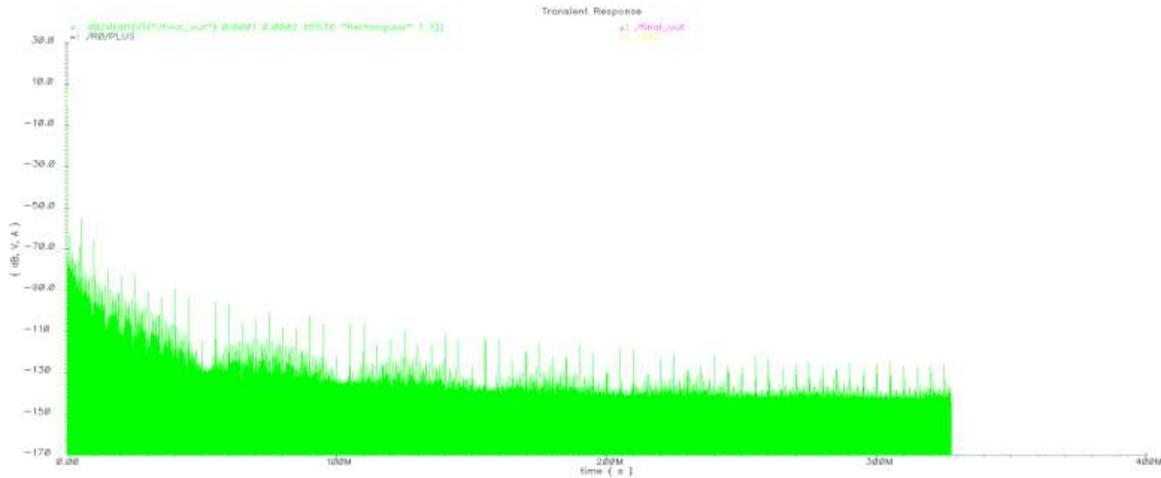


Fig. 17. FFT Output waveform of PWM controller based DC-DC Buck Converter

2) *Delta-Sigma controller based Dc-Dc Buck converter:*

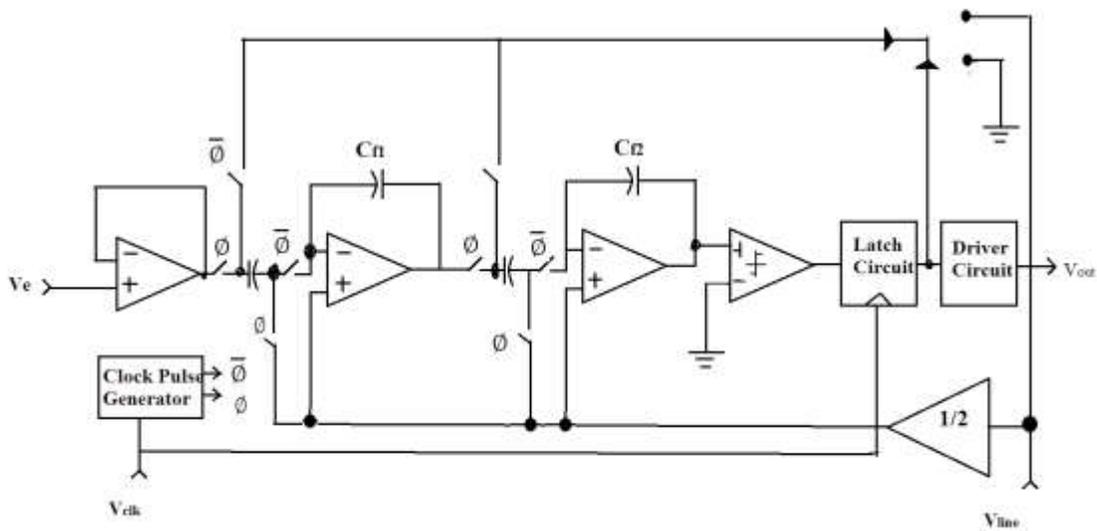


Fig. 18. Switched-capacitor  $\Delta\Sigma$  modulator

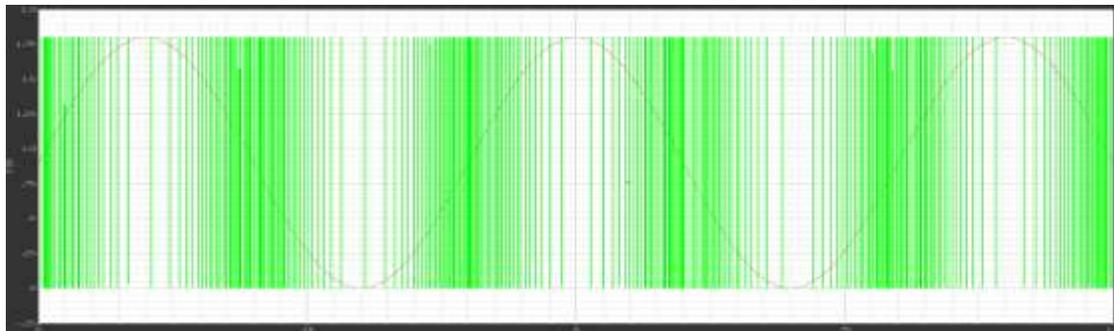


Fig. 19. Input (Sine wave) and output waveform of the delta sigma modulator

- Input Voltage range = 6V-3.9V
- Output Voltage = 3.3V

- Maximum Output Current = 943 mA
- Ripple Voltage = 6mV

Fig. 20. FFT spectra of the delta-sigma modulator-controlled dc-dc buck converter

- Frequency Component Values:

Fig. 21. FFT Plot of Delta-Sigma Modulator

- From the Plot noise shaping is clearly visible because out of band noise is shaped at rate of 40dB/decade.
- SNR = 74.87 dB

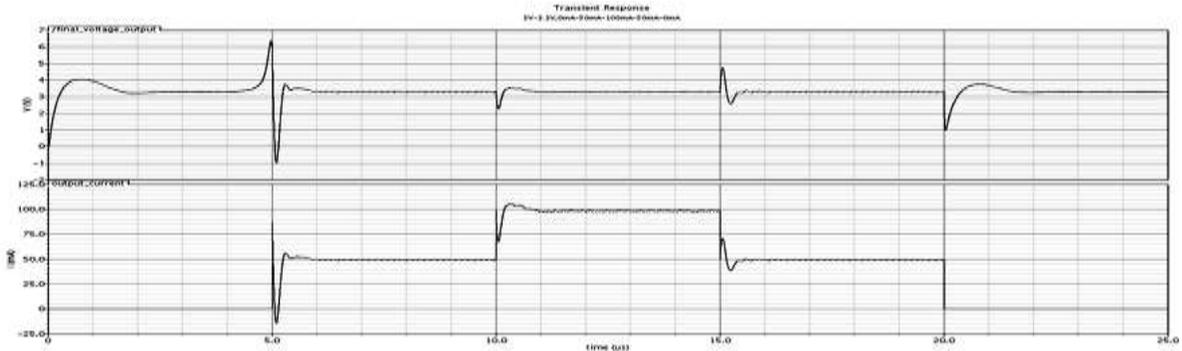


Fig. 22. Output Voltage and Current waveform for sudden switching of current 0mA→50mA→100mA→50mA→0mA for the conversion of 5V-3.3V

A. Layout

- 1) Op-amp:

Fig. 24. Op-amp Layout

- 2) Comparator:

Fig. 25. Comparator Layout

- 3) Feedback Circuits:

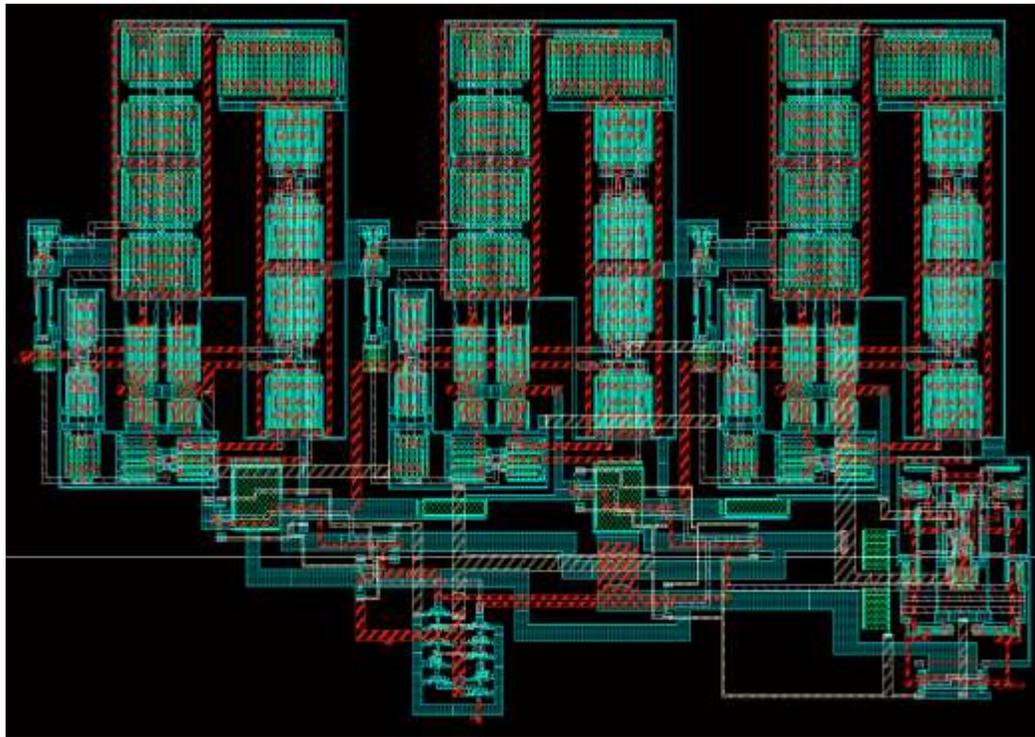


Fig. 26. Delta-Sigma Modulator Layout

4) Attenuator :



Fig. 27. Attenuator Layout

5) Level Shifter:

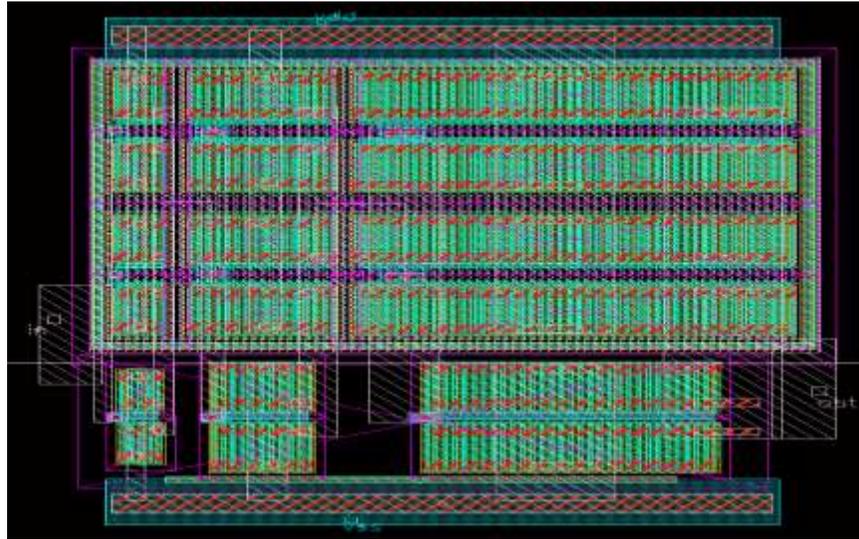


Fig. 28. Level Shifter Layout

6) Full Circuit Layout except Inductor:

Fig. 29. Layout of the Delta-Sigma modulator controlled DC-DC Buck Converter

B. Layout Verses Schematic Comparison

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Comparing attenuator_5_3.3 schematic dc_dc_layout vs attenuator_5_3.3 layout dc_dc_layout
Comparing opamp schematic opamp_layout vs opamp layout dc_dc_layout
Comparing pid_compensator schematic dc_dc_layout vs pid_compensator layout dc_dc_layout
Comparing comparator schematic dc_dc_layout vs comparator layout dc_dc_layout
Comparing not_gate schematic dc_dc_wo_esr ws not_gate layout dc_dc_wo_esr
Comparing nand_gate schematic dc_dc_wo_esr vs nand_gate layout dc_dc_wo_esr
Comparing noninverting_clock_generator schematic dc_dc_layout vs noninverting_clock_generator layout dc_dc_layout
Comparing switch_1.8 schematic dc_dc_layout vs switch_1.8 layout dc_dc_layout
Comparing del_sig_modulator schematic dc_dc_layout vs del_sig_modulator layout dc_dc_layout
Comparing level_shifter schematic dc_dc_layout vs level_shifter layout dc_dc_layout
Comparing driver_ckt schematic dc_dc_layout vs driver_ckt layout dc_dc_layout
Comparing feedback_5_3.3_wo_esr schematic dc_dc_layout vs feedback_5_3.3_wo_esr layout dc_dc_layout
Top cell full_ckt schematic dc_dc_layout ws full_ckt layout dc_dc_layout
Schematic and Layout Match
    
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Fig. 30. Layout Verses Schematic match report

C. Post Layout Simulation Result

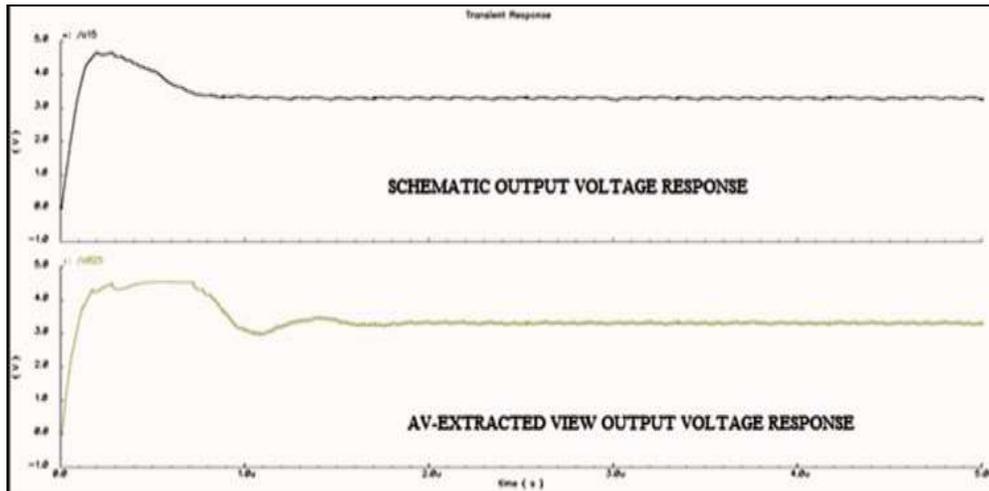


Fig. 31. Output voltage response of schematic & av-extracted view

TABLE 1. Current, Efficiency, Resistance, Ripple Voltage, and Output Voltage for 5V, 4.5V, & 4V input.

Current (mA)	Efficiency ( $\eta * 100\%$ )	Resistance (Ohms)	Ripple (mV)	Output Voltage (V)
412.543	0.846651597	8	3.319-3.291	3.300344
366.6203	0.861705703	9	3.313-3.284	3.299583
300	0.85949023	11	3.319-3.287	3.300454
275.0327	0.860514994	12	3.316-3.283	3.300392
253.8473	0.87914178	13	3.334-3.270	3.300015
235.7	0.881029275	14	3.318-3.285	3.3
219.9	0.895986612	15	3.321-3.297	3.298
164.9	0.904104811	20	3.314-3.294	3.298
143.4	0.905553609	23	3.322-3.286	3.299
131.9	0.904662042	25	3.315-3.282	3.298

V. CONCLUSION

To summarize, our study highlights the transformative impact of Delta-Sigma modulation on DC-DC Buck Converter design. By incorporating Delta-Sigma controllers and PID compensators, we have achieved unprecedented levels of efficiency and stability. Our converter boasts a peak efficiency of 91% at a high switching frequency of 200MHz, setting a new benchmark in power conversion performance. The layout, meticulously crafted to minimize mismatches using the common centroid method, ensures robustness and reliability in operation. Furthermore, the compact size of our converter facilitates seamless integration into various electronic systems, offering enhanced noise performance and regulation capabilities. This holistic approach heralds a new era in power supply technologies, with implications for a wide range of applications demanding high-performance energy conversion solutions.value.

## VI. FUTURE EXTENSION

- All the components except the inductor are on-chip. It can be replaced with switch capacitor circuit having the same functionality.
- Multi-bit Delta-sigma Modulator can be implemented to get better noise shaping in the output.
- Efficiency can be improved by implementing new design for driver, level shifter and other components.

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