Research Article

Homotopy Perturbation Analysis in an energy transit problem closed to a Stretching Surface

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ABSTRACT : Present study explored the influence of stretching constraint in addition with inclusion of energy. An analytical solution for the system of non-linear equations of motion is worked out by adopting Homotopy Perturbation method (HPM). Physical and graphical reflections various parameters are demonstrated in the present problem. Utility of this model has been perceived in diverse industrial and chemical processes. *2010 AMS subject classification: 76W05*

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Introduction

Investigation of heat transfer in boundary layer has got tremendous application in Engineering, Plasma physics etc. and become an important subject for many researchers at the present time. In 1911, Hiemenz [9] considered the 2-D fluid flow near the point of stagnation and used similarity transformation. Thereafter, mass transfer, heat transfer, stagnation point flow, different physical effects, and stagnation point, calculation of skin-friction was exercised numerous ways.

The analytic form of 2-D steady flow of incompressible fluid because of the stretch sheet was estimated by Crane [5] with varying velocity. Also, Crane and Carragher [2] discussed the transfer of heat in above given flow model. Discussion of two-dimensional flow of stagnation point on the stretch surface of an incompressible viscous fluid was initiated by Chiam [4] and Mahapatra *et al.* [12] carried out the investigation by introducing temperature distribution. The pioneer work regarding the study of *heat generation* on a stretching surface was introduced in references [2], [7], [6], [13] and carried out their research by following the different phases of the problem.

The present research includes the experiment in laminar flow in a porous media when a viscous and incompressible fluid was used on a stretch surface with generation of heat considering the stream and wall temperatures to be constant. In this proposed study, the results of Attia [1], S. Kazem *et al.* [11] were modified by employing Homotopy Perturbation Method (HPM) He J. H. [8] to obtain almost exact solution of the energy and momentum governing equations. HPM is a constructive tool to covenant with nonlinear differential equation, has been established by many authors like A. K. Jhankal [10]. Though a huge calculation is involved in this analytic method (HPM), but always provides a convenient solution to discuss the behavior of the parameters. We sketched and discussed the obtained results for discussing the heat and flow characteristics. In addition to this, the outcomes were compared with those of Attia [1] and S. Kazem *et al.* [11] to verify the accuracy of our result. Moreover, we have shown and discussed one comparison graph related to temperature with the graph obtained by Attia [1], to establish the accuracy of the method adopted here.

Mathematical formulation of the problem:

A 2-dimensional steady stagnation flow of point for an incompressible and viscous, electrically conducting fluid near O the stagnation point, on a surface which is considered along the plane y = 0 (x-axis). The substantial circumstances describing the model with initial velocity u_w , T_w be the temperature whereas

 $u_w(x)$, $T_{\infty}(x)$ are the flow velocity and temperature which are calculated externally for a boundary layer as given in Figure 1.

Figure 1: Physical model of the problem

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Figure 1: Physical model of the problem

Momentum equation, Continuity equation and the governing equation for two-dimensional steady flow, using standard boundary layer approximations Nazar *et. al.* [13], reduces "as follows:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \qquad \rightarrow (1)$$

$$\rho \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) = U \frac{dU}{dx} + \mu \frac{\partial^2 u}{\partial y^2} + \frac{\mu}{K} [U(x) - u] \qquad \rightarrow (2)$$

Where 'K' is the Darcy Permeability; μ ' is coefficient of viscosity, &' ρ ' is fluid density of a fluid. Neglecting the dissipation, the governing energy equation with the temperature vales that depends on the absorption and generation of heat as per White M. F. [14],

$$\rho C_p \left(u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right) = k \frac{\partial^2 T}{\partial y^2} + Q \left(T - T_{\infty} \right)$$
 \rightarrow (3)

Where, the symbols have their usual meaning

The boundary limitations describing the flow are given by:

$$u = u_w(x) = cx, v = 0; \ T = T_w \quad for \ y = 0$$

$$u = u_e(x) \to \alpha x; \qquad T \to T_\infty \quad for \ y \to \infty$$

Here c is any positive constant, and T_w is the temperature at the wall. Using, $v = \mu / \rho$ as kinematic viscosity, using similarity transformations:

$$u(x, y) = cxf'(\eta), \ v(x, y) = -\sqrt{cv} \ f(\eta), \ \eta = \sqrt{\frac{c}{v}} \ y, \qquad \to (5)$$

Here the prime denotes the derivative value as per the value of η . For normalizing this model of flow, the non-dimensional temperature given below is introduced:

$$\theta(\eta) = \frac{T - T_{\infty}}{T_{w} - T_{\infty}}, \operatorname{Pr} = \frac{\mu c_{p}}{K}, \ M = \frac{v}{cK}, \ C = \frac{\alpha}{c}, \ B = \frac{Q}{c\rho C_{p}} \longrightarrow (6)$$

The following nonlinear coupled differential equations are produced by applying (5), (6) in (2), (3) and

$$f'''(\eta) + f(\eta).f''(\eta) - f'^{2}(\eta) + M(C - f'(\eta)) + C^{2} = 0 \qquad \to (7)$$

$$\theta''(\eta) + \Pr.f(\eta).\theta'(\eta) + \Pr.B.\theta = 0 \qquad \to (8)$$

$$f(\eta) = 0, f'(\eta) = 1, \theta(\eta) = 1 \text{ as } \eta = 0$$

$$(9)$$

$$f'(\eta) \to C, \theta(\eta) \to 0 \qquad \text{as } \eta \to \infty \right) \qquad \to (9)$$

$$\Pr = \frac{\mu c_p}{K} \rightarrow \text{stretching parameter, } M = \frac{\nu}{cK} \rightarrow \text{porosity parameter,}$$

$$C = \frac{\alpha}{c} \rightarrow \text{stretching parameter}, B = \frac{Q}{c\rho C_p} \rightarrow \text{dim} \text{ ensionless heat generation / absorption coefficient}$$

Solution of the problem

The nonlinear coupled differential equations (7) and (8) can be rewritten as:

$$f''' + f \cdot f'' - f'^{2} - M \cdot f' + M_{1} = 0 \qquad \to (10)$$

$$\theta'' + \Pr f \cdot \theta' - M_2 \theta = 0 \qquad \rightarrow (11)$$

Constants are mentioned in the appendix

Applying HPM, the equations (10), (11) can take the following form:

$$(1-p)(f'''-M.f') + p(f'''+f.f''-f'^2-M.f') = -M_1 \longrightarrow (12)$$

$$(1-p)(\theta'' - M_2\theta) + p(\theta'' + \Pr f \cdot \theta' - M_2\theta) = 0 \qquad \rightarrow (13)$$

We consider "f" and " θ " are considered as under:

$$\begin{cases} f = f_0 + pf_1 + p^2 f_2 + \dots \\ \theta = \theta_0 + p\theta_1 + p^2 \theta_2 + \dots \end{cases}$$
 \rightarrow (14)

Using (14) in (12) and (13) and equating the terms free from 'p', the following ordinary differential equations are obtained:

$$f_0''' - M \cdot f_0' = -M_1$$
 $\to (15)$

$$\theta_0'' - M_2 \cdot \theta_0 = 0 \qquad \qquad \rightarrow (16)$$

Solving these ordinary differential equations with the boundary conditions for zeroth order i.e.,

$$f_0(o) = 0, f_0'(0) = 1, f_0'(6) = C; \theta_0(0) = 1, \theta_0(6) = 0$$
 we obtain the following solutions:

$$f_0(\eta) = C_1 + C_2 e^{\sqrt{M}\eta} + C_3 e^{-\sqrt{M}\eta} + \frac{M_1}{M}\eta \longrightarrow (17)$$

$$\theta_0(\eta) = C_4 e^{\sqrt{M_2 \eta}} + C_5 e^{-\sqrt{M_2 \eta}} \qquad \to (18)$$

Again, equating the terms involving coefficients of 'p' from the equation obtained by using (14) in (12) and (13), the following ordinary differential equations are obtained:

$$f_1''' - M \cdot f_1' + f_0 \cdot f_0'' - f_0^2 = 0 \qquad \to (19)$$

$$\theta_1'' - M_2 \theta_1 + \Pr[f_0, \theta_0'] = 0 \qquad \longrightarrow (20)$$

Solving these equations with the boundary conditions for 1st order

i.e. $f_1(o) = 0$, $f_1'(0) = 0$, $f_1'(6) = 0$; $\theta_1(0) = 0$, $\theta_1(6) = 0$ we obtain the following solutions:

$$f_{1}(\eta) = C_{6} + C_{7}e^{\sqrt{M}\eta} + C_{8}e^{-\sqrt{M}\eta} + A_{10}\eta^{2} + A_{11}\eta^{3} + A_{12}\eta - \left[A_{15}e^{2\sqrt{M}\eta} - A_{16}e^{-2\sqrt{M}\eta}\right] - \eta\left[E_{1}e^{\sqrt{M}\eta} + E_{2}e^{-\sqrt{M}\eta}\right] + \eta^{2}\left[A_{17}e^{\sqrt{M}\eta} + A_{18}e^{-\sqrt{M}\eta}\right] \rightarrow (21)$$

$$\theta_{1}(\eta) = C_{9}e^{\sqrt{M_{2}\eta}} + C_{10}e^{-\sqrt{M_{2}\eta}} + \eta\left[A_{39}e^{\sqrt{M_{2}\eta}} + A_{40}e^{-\sqrt{M_{2}\eta}}\right] - \eta^{2}\left[A_{35}e^{\sqrt{M_{2}\eta}} - A_{36}e^{-\sqrt{M_{2}\eta}}\right] - \left[A_{31}e^{M_{3}\eta} - A_{32}e^{-M_{3}\eta}\right] + \left[A_{39}e^{M_{4}\eta} - A_{34}e^{-M_{4}\eta}\right] \rightarrow (22)$$

Neglecting higher order perturbed terms we finally obtain:

$$\begin{split} f(\eta) &= f_0 + p f_1 \\ &= C_1 + C_2 e^{\sqrt{M}\eta} + C_3 e^{-\sqrt{M}\eta} + \frac{M_1}{M} \eta \\ &+ p \begin{pmatrix} C_6 + C_7 e^{\sqrt{M}\eta} + C_8 e^{-\sqrt{M}\eta} + A_{10}\eta^2 + A_{11}\eta^3 + A_{12}\eta - \left[A_{15} e^{2\sqrt{M}\eta} - A_{16} e^{-2\sqrt{M}\eta}\right] \\ &- \eta \left[E_1 e^{\sqrt{M}\eta} + E_2 e^{-\sqrt{M}\eta}\right] + \eta^2 \left[A_{17} e^{\sqrt{M}\eta} + A_{18} e^{-\sqrt{M}\eta}\right] \end{pmatrix} \end{split}$$

And,

$$\begin{aligned} \theta(\eta) &= \theta_0 + p \,\theta_1 \\ &= C_4 e^{\sqrt{M_2}\eta} + C_5 e^{-\sqrt{M_2}\eta} \\ &+ p \begin{pmatrix} C_9 e^{\sqrt{M_2}\eta} + C_{10} e^{-\sqrt{M_2}\eta} + \eta \Big[A_{39} e^{\sqrt{M_2}\eta} + A_{40} e^{-\sqrt{M_2}\eta} \Big] - \eta^2 \Big[A_{35} e^{\sqrt{M_2}\eta} - A_{36} e^{-\sqrt{M_2}\eta} \Big] \\ &- \Big[A_{31} e^{M_3\eta} - A_{32} e^{-M_3\eta} \Big] + \Big[A_{33} e^{M_4\eta} - A_{34} e^{-M_4\eta} \Big] \end{pmatrix} \end{aligned}$$

The terminologies for viscous drag (τ) and Nusselt number (Nu) are articulated as:

$$\tau = \left(\frac{\partial f}{\partial \eta}\right)_{\eta=0} = \sqrt{M}(C_2 - C_3) + \frac{M_1}{M} + p\left[\sqrt{M}(C_7 - C_8) + A_{12} - 2\sqrt{M}(A_{15} + A_{16}) - (E_1 + E_2)\right]$$

Nu = $-\left(\frac{\partial \theta}{\partial \eta}\right)_{\eta=0} = -\sqrt{M_2}(C_4 - C_5) - p\left[\sqrt{M_2}(C_9 - C_{10}) + A_{39} + A_{40} - M_3(A_{31} + A_{32}) + M_4(A_{33} + A_{34})\right]$

Findings

The present analysis reveals the expressions of boundary layer equations with *viscous drag* and *Nusselt number* are piled up to get a variety of graphs with their substantial interprtations by taking some standard values of different parameters implicated in the problem.







Figure 3: Velocity $f'(\eta)$ versus η under , M = 3, p = 0.1 Effect of parameter C on velocity f'

Figures 2 and 3 demonstrate the impact of stretch parameter on the profile of the velocity. The f and f' velocity profiles areaccelerated for different values of stretching parameter (C = 0.5, 1, 1.5). Furthermore, both the figure shows the fact that the velocity distribution is directly proportional to the stretching parameter C.



Figure 4: Température $\Theta(\eta)$ versus η Under M = 1, Pr = 0.7, |B| = 0.1, P = 0.1 *Effect of parameter C on* Θ



Figure 5: Température $\Theta(\eta)$ versus η Under M=0.5, Pr =0.7, |B|=0.1, P = 0.1 Effect of parameter C and B on Θ

Figures 4 depicts the consequence of stretching parameter on profile of temperature. It was noted that temperature profile continuously reduced for varying the stretching parameter (C = 0.5, 1, 1.5) i.e. the temperature distribution is continuously moves down on account of stretching parameter.

Figure 5, shows the temperature profile for differentparameter values for heat generation and stretching parameter. It was observed that fluid temperature of the present flow problem is enlarged for boosting the heat generation which clearly satisfies the physical reality.



Figure 6: Temperature versus η under M=1, Comparison of results 0.1, P=0.1 Effects of parameter Pr and C on the profile of θ



Figure 7 : (Fig 5 of H. A. Attia[9]): Temperature versus η under M = 1, |B| = 0.1

For comparing the results of the present research, the experiment of H. A. Attia [1] was considered. When figure 6 and 7 were compared (Figure 5 of the work done by H. A. Attia [1]), we observed the same kind of behavior due to the effects of Pr and C on temperature profile for fixed M = 1 and |B| = 0.1. i.e., there is a

significant impact of Prandtl number on thickness of thermal boundary layer. Higher value of Pr lower is the thickness for consequent number of stretching parameter. Similarly, the fluid temperature falls for enhancing values of stretching parameter. Thus, an excellent agreement exists among the results achieved by H. A. Attia [1] and the present authors.

Concluding remarks

- (a) The velocity distribution is directly proportional to the stretching parameter.
- (b) The temperature distribution is continuously moves down on account of stretching parameter.
- (c) The fluid temperature is enlarged for boosting the heat generation.
- (d) High Prandtl number values condensed the thickness of thermal boundary layer for consequent values of stretching parameter.

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<u>Appendix</u>

- $M_1 = C.(C + M)$ $M_2 = -\Pr B$ $M_3 = \sqrt{M} + \sqrt{M_2}$ $M_4 = \sqrt{M} - \sqrt{M_2}$ $M_5 = \frac{M_1}{M} - 1$
- $C_{1} = -C_{2} C_{3}$ $C_{2} = C_{3} \frac{M_{5}}{\sqrt{M}}$ $C_{3} = \frac{M_{5}e^{6\sqrt{M}} \frac{M_{1}}{M} + C}{\sqrt{M} \left(e^{6\sqrt{M}} e^{-6\sqrt{M}}\right)}$ $C_{4} = \frac{1}{1 e^{12\sqrt{M_{2}}}}$ $C_{5} = -C_{4}e^{12\sqrt{M_{2}}}$ $A_{1} = 2C_{2}C_{3}M 2C_{2}C_{3} C_{1}^{2}$ $A_{2} = -2C_{1}\frac{M_{1}}{M}$ $A_{3} = -\frac{M_{1}^{2}}{M^{2}}$ $A_{4} = C_{1}C_{2}(M 2)$ $A_{5} = C_{1}C_{3}(M 2)$ $A_{6} = C_{2}^{2}(M 1)$ $A_{7} = C_{3}^{2}(M 1)$
- $A_{8} = C_{2}M_{1}(1 \frac{2}{M}) \qquad A_{9} = C_{3}M_{1}(1 \frac{2}{M}) \qquad A_{10} = \frac{A_{2}}{2M}$ $A_{11} = \frac{A_{3}}{3M} \qquad A_{12} = \frac{1}{M}(A_{1} + \frac{2A_{3}}{M}) \qquad A_{13} = \frac{A_{4}}{2M}$

 $A_{14} = \frac{A_5}{2M}$ $A_{15} = \frac{A_6}{\epsilon M \sqrt{M}}$ $A_{16} = \frac{A_7}{6M\sqrt{M}}$ $A_{17} = \frac{A_8}{4M}$ $A_{18} = \frac{A_9}{4M}$ $A_{19} = \frac{3A_8}{4M_1/M_1}$ $A_{20} = \frac{3A_9}{4M_4/M}$ $E_1 = A_{13} - A_{19}$ $E_2 = A_{14} + A_{20}$ $E_4 = \frac{-A_{12} + 2\sqrt{M}(A_{15} + A_{16}) + (E_1 + E_2)}{\sqrt{M}}$ $E_3 = A_{15} - A_{16}$ $E_{5} = -\frac{12A_{10} + 108A_{11} + A_{12}}{\sqrt{M}} + 2(A_{15}e^{12\sqrt{M}} + A_{16}e^{-12\sqrt{M}}) + 6(E_{1}e^{6\sqrt{M}} - E_{1}e^{-6\sqrt{M}})$ $+\frac{1}{\sqrt{M}}(E_{1}e^{6\sqrt{M}}+E_{2}e^{-6\sqrt{M}})-36(A_{17}e^{6\sqrt{M}}-A_{18}e^{-6\sqrt{M}})-\frac{12}{\sqrt{M}}(A_{17}e^{6\sqrt{M}}+A_{18}e^{-6\sqrt{M}})$ $C_{7} = \frac{E_{5} - E_{4}e^{-6\sqrt{M}}}{e^{6\sqrt{M}} - e^{-6\sqrt{M}}} \qquad \qquad C_{8} = \frac{E_{5} - E_{4}e^{6\sqrt{M}}}{e^{6\sqrt{M}} - e^{-6\sqrt{M}}}$ $C_6 = E_3 - C_7 - C_8$ $A_{21} = \Pr.C_1.C_4.\sqrt{M_2}$ $A_{22} = \Pr.C_1.C_5.\sqrt{M_2}$ $A_{23} = \Pr.C_2.C_4.\sqrt{M_2} \qquad A_{24} = \Pr.C_3.C_5.\sqrt{M_2} \qquad A_{25} = \Pr.C_2.C_5.\sqrt{M_2}$ $A_{26} = \Pr.C_3.C_4.\sqrt{M_2} \qquad A_{27} = \Pr.C_4.\frac{M_1\sqrt{M_2}}{M} \qquad A_{28} = \Pr.C_5.\frac{M_1\sqrt{M_2}}{M}$ $C_{9} = \frac{B_{2} - B_{1}e^{-6\sqrt{M_{2}}}}{e^{6\sqrt{M_{2}}} - e^{-6\sqrt{M_{2}}}} \qquad C_{10} = \frac{B_{1}e^{6\sqrt{M_{2}}} - B_{2}}{e^{6\sqrt{M_{2}}} - e^{-6\sqrt{M_{2}}}} \qquad B_{1} = A_{31} - A_{32} - A_{33} + A_{34}$ $B_{2} = -6(A_{39}e^{6\sqrt{M_{2}}} + A_{40}e^{-6\sqrt{M_{2}}}) + 36(A_{35}e^{6\sqrt{M_{2}}} - A_{36}e^{-6\sqrt{M_{2}}}) + (A_{31}e^{6M_{3}} - A_{32}e^{-6M_{3}}) - (A_{33}e^{6M_{4}} - A_{34}e^{-6M_{4}}), \quad A_{29} = \frac{A_{21}}{2\sqrt{M_{2}}}$ $A_{30} = \frac{A_{22}}{2\sqrt{M}} A_{31} = \frac{A_{23}}{M_2^2 - M_2}, \qquad A_{32} = \frac{A_{24}}{M_2^2 - M_2}$ $A_{33} = \frac{A_{25}}{M_4^2 - M_2} \qquad \qquad A_{34} = \frac{A_{26}}{M_4^2 - M_2}$ $A_{36} = \frac{A_{28}}{4\sqrt{M_2}}$ $A_{37} = \frac{A_{27}}{4M}$ $A_{35} = \frac{A_{27}}{4\sqrt{M_{27}}}$ $A_{39} = -A_{29} + A_{37}$ $A_{38} = \frac{A_{28}}{4M}$ $A_{40} = -A_{30} - A_{38}$